



**Interconnection Feasibility Study Report
GIP-080-FEAS-R2**

**Generator Interconnection Request #80
30MW Wind Generating Facility
Cumberland (L-5550), NS**

August 17, 2007
Control Centre Operations
Nova Scotia Power Inc.

Executive Summary

A feasibility study was conducted in response to Interconnection Request number 080 (IR080) which proposes to connect 30 MW of wind powered generation in Cumberland Co., Nova Scotia. The customer has requested NRIS service. This facility would connect to the transmission system at a location 11 km from Parrsboro on line L-5550.

At the proposed Point of Interconnection (POI) the system was found to have sufficient strength (short-circuit) and thermal capacity to accommodate the addition of the full capacity of this generating facility. The direct interconnection costs of the 69 kV interconnection are estimated to be \$1.8 million with a 12 to 24 month time to construct. However, projects that precede this project in the Generation Interconnection Queue (Queue) may utilize most of the 69 kV transmission capacity available and thereby reduce the capacity available to IR080. Alternatively a 138 kV interconnection can be provided, which will accommodate the full 30 MW capacity, with an estimated direct interconnection cost of \$3.6 million and a 12 to 24 month time to construct. The interconnection costs are provided in section 10.

Generating facilities added to the system in northern Nova Scotia (between Truro and New Brunswick) can have an impact on the transfer capability between Nova Scotia and New Brunswick and the special protection systems (SPS) that have been installed to facilitate those transfers. This project will necessitate upgrading these SPSs but allocation of those costs are dependent on whether projects that are ahead of this project in the Queue proceed. These costs are identified as indirect or to be determined (TBD) in section 10. A discussion regarding these transfer capabilities and the SPSs is included in section 8.

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1 Introduction

The Interconnection Customer submitted an Interconnection Request to NSPI for a proposed 30 MW wind generation facility interconnected to the NSPI's 69 kV line L-5550. The Point of Interconnection (POI) will be approximately 11 km from NSPI's 37N-Parrsboro substation on L-5550. The Interconnection Customer signed a Feasibility Study Agreement to study the connection of their proposed generation to the NSPI transmission system. This report is the result of that Study Agreement. The Interconnection Customers (IC) substation would be located adjacent to L-5550 and not require any new 69 kV line construction to interconnect. An alternate 138 kV POI was added to this study at the discretion of NSPI.

2 Scope

The Interconnection Feasibility Study (FEAS) report shall provide the following information:

- i) preliminary identification of any circuit breaker short circuit capability limits exceeded as a result of the interconnection;
- ii) preliminary identification of any thermal overload or voltage limit violations resulting from the interconnection; and
- iii) preliminary description and non-binding estimated cost of facilities required to interconnect the Generating Facility to the Transmission System, the time to construct such facilities, and to address the identified short circuit and power flow issues.

The scope of this FEAS includes modeling the power system in normal state (with all transmission elements in service) under anticipated load and generation dispatch conditions.

For Energy Resources Integration Service (ERIS), if the FEAS determines that transmission upgrades are required as a result of thermal overload, voltage violation, or equipment rating, then the FEAS will determine the amount of generation that can be installed without necessitating major transmission upgrades. The FEAS will provide a preliminary high level cost estimate of the direct interconnection costs.

For NRIS service type, the FEAS will identify any transmission upgrades required as the result of thermal overload, voltage violation, or equipment rating. The FEAS will attempt to provide high level cost estimates for such upgrades and the direct interconnection costs.

A more detailed analysis of the technical implications of this development will be included in the System Impact Study (SIS) report. This may include system stability

analysis, single or double contingencies, off-nominal frequency operation, off-nominal voltage operation, low voltage ride through, harmonic current distortion, harmonic voltage distortion, system protection, special protection system (SPS), automatic generation control (AGC) and islanded operation. The impacts on neighboring power systems and the requirements set by reliability authorities such as Northeast Power Coordinating Council (NPCC), North American Reliability Council (NERC), and Nova Scotia Power (NSPI) will be addressed at that time. The SIS may identify additional costs and upgrades that were not identified in this FEAS.

As well, a separate Facility Study will follow the SIS in order to ascertain the final cost estimate for the transmission upgrades requirement.

3 Assumptions

The POI and configuration studied are as follows:

- i) 30 MW wind farm comprised of 15 – 2.0 MW Enercon E82 wind turbines and has requested NRIS service.
- ii) The wind generating facility is located 11 km from the 37N-Parrsboro 69 kV substation immediately adjacent to L-5550.
- iii) Transformer Impedance assumed at 7% (on ONAN Base), rated 24/32 MVA.

This feasibility study is based on the assumption that projects that are ahead of this project in the Generation Interconnection Queue (Queue) will not proceed but impacts are reviewed qualitatively.

4 Projects With Higher Queue Positions

As of 30 June 2007 the following projects can proceed ahead of this project, due to their position in the Queue, and have the status indicated.

In-service and committed generation projects

- Wind Generation - 30.5 MW - connected to L-5027 (in-service)
- Wind Generation – 15 MW – connected to L-5573 (in-service)
- Wind Generation – 20 MW - distribution connected (in-service)
- Wind Generation – 40 MW – distribution connected (committed)

Generation projects with a higher Queue position, not yet committed

- IR008 Wind – Guysborough (L-5527B) 15 MW NRIS – FAC complete
- IR017 Wind – Lunenburg (L-6004) 100 MW NRIS- FEAS complete
- IR023 Wind – Inverness (L-6549) 100 MW NRIS - FEAS complete
- IR042 Wind – Cape Breton (Victoria Junction) 100 MW NRIS- FEAS complete

- IR044 Wind – Colchester (L-6503) 35 MW NRIS- FEAS complete
- IR045 Wind – Cumberland (L-6535) 35 MW NRIS- SIS complete
- IR046 Wind – Colchester (L-6513) 32 MW ERIS- FEAS complete
- IR056 Wind – Cumberland (L-5058) 60 MW ERIS- FEAS complete
- IR067 Wind – Annapolis (L-5026) 32 MW ERIS- FEAS in progress
- IR068 Wind – Digby (L-6513) 32 MW ERIS- FEAS in progress
- IR072 Wind – Guysboro (L-6515) 100 MW NRIS- FEAS in progress
- IR079 Wind – Antigonish (L-6515) 50 MW NRIS- FEAS in progress

This project and projects IR045, 46 and 56 add generation to transmission facilities that are part of the Nova Scotia to New Brunswick interconnection. These projects will compete for transmission capacity. This project and project IR056 will both connect to the same 69 kV system and may impact each other. The remaining projects may have an impact on this project in that all projects will require use of transmission facilities to deliver power to the load centers.

The SIS will be based on the assumption that all projects that are ahead of this project in the Queue are in-service. Should any project that is ahead of this project be withdrawn, or changed, within the established procedures then the SIS for this project must be updated accordingly, at the project proponents expense.

5 Short-Circuit Duties

The maximum (future) expected short-circuit level on 69kV systems is 3500MVA.

The short-circuit levels in the area before and after this development are provided in Table 6-1 below.

Table 5-1: Short-Circuit Levels. Three-phase MVA (1)		
Location	This project not in service	This project in service
All transmission facilities in service – 138 kV Interconnection		
30N-Maccan - 138 kV	1060	1120
L-5550 Tap– 138 kV(2)	675	740
L-6514 Springhill to Maccan Out of Service – 138 kV Interconnection		
30N-Maccan - 138 kV	620	685
L-5550 Tap – 138 kV(2)	460	523

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All transmission facilities in service – 69kV Interconnection		
30N-Maccan - 69 kV	365	424
69 kV L-5550 Tap – 69 kV(2)	201	269
Maccan 138/69 kV Transformer Out of Service – 69 kV Interconnection		
30N-Maccan - 69 kV	198	257
L-5550 Tap - 69 kV(2)	138	206

(1) Classical fault study

(2) POI

In determining the maximum short-circuit levels with this generating facility in service the generators have been modeled as conventional machines with reactance comparable to induction machines regardless of the type of generators proposed. This provides a worst case estimation.

The maximum short-circuit level on the 30N-Maccan 69kV bus is presently 365 MVA. Although the actual increase in short-circuit levels will be dependent on the specific type of generator installed, the addition of this facility will not cause any significant contribution to short-circuit level regardless of the type of generator selected. Changes to protection systems at the Maccan terminal of L-5550 can be expected to maintain protection coordination. To maintain customer service reliability a line terminal breaker will be installed at 30N-Maccan, terminating L-5550.

6 Thermal Limits

The 69 kV line L-5550 serves to transmit power from 30N-Maccan to 37N-Parrsboro. The conductor is rated 82 and 54 MVA for winter and summer conditions respectively. The relaying at the Maccan terminal, limits the line to 29 MVA. As this line has been constructed to 138 kV standards it is expected that this line, in fact, has a much higher capability. The relaying at Maccan can be changed to facilitate the connection of this customer's facility.

Line L-5029 connects the Springhill substation with the 30N-Maccan substation. The substations at 30N-Maccan and 74N-Springhill contain one 138/69 kV transformer each. These transformers have maximum thermal ratings of 56 MVA and both serve local distribution loads as well as the 69 kV system. To provide service reliability to customers in the areas of Pugwash, Oxford, Springhill and Amherst the 138/69 kV transformers at 74N-Springhill and 30N-Maccan provide alternate sources for the 69 kV system in the event that one transformer should fail or have to be removed from service for maintenance. In order to permit removal or loss of one of these transformers, without curtailing generation, either the total generation connected to the 69 kV systems (Maccan and Springhill) must be limited to 50 MW or the system reinforced. The system can be reinforced by adding 138/69 kV transformer capacity. Alternatively the generation may be connected to the 138 kV system.

This project is feasible at the full requested capacity without such upgrades provided that IR056 does not proceed or does not install more than 20 MW of capacity. These two projects are both connected to the 69 kV system and therefore must not exceed 50 MW in total.

The requirement for restrictions or curtailments of this facility when operating with an element (transmission line, transformer, bus etc) out of service (N-1 operation) will be further assessed in the SIS.

This generating facility will require a curtailment scheme and high speed rejection scheme for integration with NSPI SCADA controls and SPSs) to maximize the capability of NSPIs transmission system, system security, and production of all generating facilities.

7 Voltage Control

The ratio of 69 kV short-circuit level to generating capacity under system normal conditions is 6.7 (201/30). With this ratio voltage control voltage and voltage flicker will be acceptable. With the Maccan 138/69 kV transformer out of service the ratio of short-circuit level to generating capacity is 4.6 (138/30). For this condition the voltage flicker generated, specific to the machine selected, will be assessed in the SIS.

The facilities included with this installation must be such that the facility is capable of providing both lagging and leading power factor of 0.95, measured at the high voltage (transmission) connection point, when the facility is delivering full power. A centralized controller will be required which adjusts individual generator real and reactive power output, in real time, and regulate the voltage at the high-voltage (transmission) connection point. The voltage controls must be responsive to voltage deviations at the connection point, be equipped with a voltage set-point control, and also have facilities that will slowly adjust the set-point over several minutes (5-10) to maintain reactive power just within the individual generators capabilities. The latter control may be referred to as a slow-Q control. Details of the specific control features, control strategy and settings will be reviewed and addressed in the SIS.

NSPI must have manual and remote control of the voltage set-point, the slow-Q controls and reactive power output from this facility.

This facility must also have low-voltage ride-through capability. The SIS will verify this and state any specific options, controls and additional facilities that are required to achieve this.

8 System Limitations (Transfer Capability)

The existing Nova Scotia import capability, measured at the Nova Scotia – New Brunswick border, is limited to the lesser of 300 MW or 22% of load. This is the maximum import that can be scheduled across the Nova Scotia – New Brunswick interface with all facilities in service. In addition, when Nova Scotia is importing 300 MW the loss of the largest NSPI generating contingency (two units) will increase the import level an additional 328 MW to 628 MW. The Nova Scotia Power System operator will then return the import level to 300 MW as quickly as possible and within 30 minutes of the generation loss. This is achieved by loading generation reserves and, if necessary, shedding load. Thus the system must be capable of operating with a Nova Scotia import of 300 MW and the subsequent loss of 328MW of generation and with acceptable voltages and all facilities within their thermal capabilities. As generation is added in northern Nova Scotia transmission reinforcement will be required in order to maintain this transmission capability. L-6513 is the limiting transmission facility with a summer thermal rating of 110 MVA. When the generation installed in northern Nova Scotia exceeds 60 to 90 MW (depending on location) upgrading of L-6513 will be required or a second 138 kV line be constructed. Alternatively the two unit contingency can be removed by adding a circuit breaker at 50N-Trenton and reconfiguring the 88S-Lingan bus. If projects that are ahead of this project in the Queue proceed, then this project may cause overloading of L-6513, following this contingency, thereby necessitating upgrades to line L-6513.

The existing Nova Scotia export capability, measured at the Nova Scotia – New Brunswick border, is 300 MW but can be increased to 350 MW under certain operating conditions. NSPI has a commitment to hold portion of the total export capability in reserve, on a long term basis, as part of its reserve sharing agreement with the New Brunswick System Operator (NBSO). With all facilities in service and a 350 MW export, all facilities must be loaded within their thermal capabilities and with acceptable system voltages.

NSPI has made extensive use of Special Protection Systems (SPS) in order to reduce/avoid capital expenditures and improve overall cost efficiencies. These systems act to maintain system stability and remove equipment overloads, post contingency, by rejecting generation and/or shedding load. NSPI continues to have no objection to the application of such systems to reduce interconnection costs. However, these systems must be designed, installed and periodically tested in accordance with criteria, guidelines and procedures that are set forth by reliability organizations which include NSPI, NPCC and NERC. The application, design, maintenance and testing of SPSs must comply with all present and future requirements. The NSPI system has several congested interfaces (transmission corridors that are regularly operated at limits). NSPI has made use of SPS to increase transfer limits on these interfaces. There are practical limits to the amount of generation and load that can be rejected by SPSs and the amount of generation that can be

curtailed following a single contingency loss before system stability and reliability are compromised.

There are a number of SPSs and protective systems employed by NSPI and the NBSO to permit these high transfer levels between the two systems. NSPI has an “Import Power Monitor” that acts to separate the two systems following the loss of the 345 kV tie (L-8001/L-3025), by cross-tripping L-6513. Currently this system is armed when imports exceed 100MW. Once this SPS operates, the load and generation in northern Nova Scotia are disconnected from the Nova Scotia system (but remain connected to New Brunswick). The Nova Scotia system is then islanded and relies on under frequency load shedding (UFLS) schemes to shed load across Nova Scotia to make up the generation deficiency and restore balance. As generation is located in northern Nova Scotia, unless changes are made to this SPS, the scheme will be compromised (as will the Nova Scotia import capability) as it will disconnect generation resources (in northern NS) from the NSPI system. When generation in this area exceeds 40 MW, this SPS will as a minimum, have to be modified by relocating the system separation point from L-6513 at Onslow to the NB border (Maccan and Memramcook). When the generation in northern Nova Scotia exceeds 125 MW then either L-6513 must be thermally upgraded or an additional 138 kV line constructed. Stability and ride-through capability of generation in this area will be critical. This import SPS can also be triggered by a number of SPSs in New Brunswick for contingencies near Memramcook and Salisbury.

When NSPI is exporting power such that the loss of L-8001/L-3025 will result in thermally overloading L-6513 (NS export approximately 100 MW) the “NS Export Power Monitor” is armed. Should L-8001 trip, then this SPS will reject generation in eastern Nova Scotia to ensure that L-6513 is not thermally overloaded and does not trip. We do not expect this project, in addition to projects that precede it in the Queue, to compromise this SPS.

There are a number of proposed generation additions in New Brunswick that may have an impact on projects in northern NS and visa versa. Their POI, size and relative position of the NS and NB interconnection Queues will determine the impact. This will be resolved through collaboration with NBSO at the SIS stage.

As the penetration of wind generation increases in this area it is expected that the reliance on the existing SPS scheme may compromise system security. This will depend on the amount of wind and its variability. At some level we expect either this SPS scheme will be redesigned or transmission expansions required for system security. The transmission expansions, if required, may include a second 138 kV transmission line between 1N-Onslow and 74N-Springhill. This requirement will be determined by the SIS.

This generating facility will also increase loading on the Onslow South corridor (Truro to Halifax) by replacing generation south and west of Truro. This may require increased reactive support requirements in the Halifax area or invoke facility additions that can reduce the reactive support requirements. This will be evaluated in the SIS.

The SIS will determine the facility changes that are required to permit higher transmission loadings while maintaining compliance with NERC/NPCC standards and in keeping with good utility practices.

9 Expected Facilities Required for Interconnection

Based on the above discussion we expect that it will be feasible to interconnect this facility with 30 MW or less, to the 69 kV system as requested without reinforcing the 69 kV system provided that the total capacity of this project and IR056 does not exceed 50 MW. Should reinforcements be required then the alternatives are to add 138/69 kV transformer capacity or interconnect this facility at 138 kV by converting L-5550 to 138 kV.

Therefore we have provided two estimates for interconnection at 69 kV or 138 kV.

69 KV Interconnection L-5550 – 30 MW or less

Additions/Changes to NSPI systems

- i) Replace protection on L-5550 and L-5029 at Maccan
- ii) Install 69 kV line terminal at 30N-Maccan on L-5550
- iii) Install transfer trip between the L-5550 protection at 30N-Maccan and the IC substation.
- iv) Control and Communications between the IC substation, Maccan & NSPI SCADA system (to be specified)
- v) Inclusion of generating facility into NSPIs generation rejection SPSs and load curtailment schemes
- vi) Relocation of separation point for the “NS Import Power Monitor” from the 1N-Onslow terminal of L-6513 to the 30N-Maccan terminal of L-6535 and the Memramcook terminal of L-6536. Should IR045 proceed then the SPS would be moved to that POI substation rather than Maccan. This may not be required depending on the status of preceding projects in the Queue.
- vii) Install circuit breaker at 50N-Trenton and reconfigure the 88S-Lingan bus. This may not be required depending on the status of preceding projects in the Queue
- viii) Upgrade L-6513 to 60C. This may not be required depending on the status of preceding projects in the Queue

Additions/Changes to be included at the IC’s Interconnection Facilities:

- ix) 69 kV IC Substation. This will be constructed for 138 and 69 kV operation. This will include 69 kV circuit breaker and protections as acceptable to NSPI, An

RTU to interface with NSPIs SCADA with telemetry and controls as required by NSPI. NSPI will require real-time monitoring of the IC substation.

- x) Facilities to provide 0.95 leading and lagging power factor when delivering rated output (30 MW) all at the 69kV IC point when the voltage at that point is operating between 95 and 105 % of nominal.
- xi) Centralized controls. These will provide centralized voltage set-point controls and slow-Q controls which acts to control the voltage on the 69 kV system and the reactive output of the machines. Responsive (fast-acting) controls are required. The controls will also include a curtailment scheme which will limit or reduce total output from the facility, upon receipt of a telemetered signal from NSPIs SCADA system. The controller will also limit the load ramp rate of the facility to within limits set by NSPI and/or telemetered from NSPIs SCADA system.
- xii) NSPI to have control and monitoring of reactive output of this facility, via the centralized controller. This will permit the NSPI operator to raise or lower the voltage set-point and change the status of any slow-Q controls, remotely. NSPI will also have remote manual control of the load curtailment scheme.
- xiii) Low voltage ride-through capability
- xiv) Facilities for NSPI to execute high speed rejection of generation (transfer trip)
- xv) Accessible and tree-cleared lands or Rights Of Way (ROW) acceptable to NSPI for design and construction of any required new transmission line or Transmission Provider's substation.

b) 138 KV Interconnection Maccan – 30 MW

Additions/Changes to NSPI systems

- i) Convert L-5550 to 138 kV and terminate at 30N-Maccan
- ii) Install 138 kV circuit breaker and line terminal at 30N-Maccan
- iii) Install transfer trip between the L-5550 protection at 30N-Maccan and the IC substation.
- iv) Convert 37N-Parrsboro substation to 138 kV. This requires replacing the 69/25 kV 7.5/10//11.2 MVA transformer and miscellaneous apparatus with equipment rated for 138 kV operation
- v) Control and Communications between IC substation, Macan & NSPI SCADA system (to be specified)
- vi) Inclusion of generating facility into NSPIs generation rejection SPSs and load curtailment schemes

- vii) Relocation of separation point for the “NS Import Power Monitor” from the 1N-Onslow terminal of L-6513 to the 30N-Maccan terminal of L-6535 and the Memramcook terminal of L-6536. Should IR045 proceed then the SPS would be moved to that location rather than Maccan. This may not be required depending on the status of preceding projects in the Queue
- viii) Install circuit breaker at 50N-Trenton and reconfigure the 88S-Lingan bus. This may not be required depending on the status of preceding projects in the Queue
- ix) Upgrade L-6513 to 60C. This may not be required depending on the status of preceding projects in the Queue

Additions/Changes to be included at the IC’s Interconnection Facilities:

- x) 138 kV IC Substation. This will include 138 kV circuit breaker and protections as acceptable to NSPI, An RTU to interface with NSPIs SCADA with telemetry and controls as required by NSPI. NSPI will require real-time monitoring of the IC substation.
- xi) Facilities to provide 0.95 leading and lagging power factor when delivering rated output (30 MW) all at the 138kV POI when the voltage at that point is operating between 95 and 105 % of nominal.
- xii) Centralized controls. These will provide centralized voltage set-point controls and slow-Q controls which acts to control the voltage on the 138 kV system and the reactive output of the machines. Responsive (fast-acting) controls are required. The controls will also include a curtailment scheme which will limit or reduce total output from the facility, upon receipt of a telemetered signal from NSPIs SCADA system. The controller will also limit the load ramp rate of the facility to within limits set by NSPI and/or telemetered from NSPIs SCADA system.
- xiii) NSPI to have control and monitoring of reactive output of this facility, via the centralized controller. This will permit the NSPI operator to raise or lower the voltage set-point and change the status of any slow-Q controls, remotely. NSPI will also have remote manual control of the load curtailment scheme.
- xiv) Low voltage ride-through capability
- xv) Facilities for NSPI to execute high speed rejection of generation (transfer trip)
- xvi) Accessible and tree-cleared lands or Rights Of Way (ROW) acceptable to NSPI for design and construction of any required new transmission line or Transmission Provider's substation.

10 Magnitude of NSPI Interconnection Facilities Cost Estimate

a) 69 KV Interconnection L-5550 – Generating Capacity to 15-30 MW

Direct Interconnection Cost Items	Estimate
i) Upgrade protection L-5550 and L-5029 at Maccan	200,000
ii) Install 69 kV line terminal	800,000
iii) Control & Communications between NSPI and customer	500,000
iv) Additions and changes to NSPI SPSs (NSPI costs only)	100,000
v) Contingency (10%)	160,000
Total of Direct Interconnection Costs	1,760,000
Indirect Cost Items (To Be Determined)	TBD (SIS)
vi) Upgrade L-6513 to 60C (32 km)	500,000
vii) Relocate NSPI Import Power SPS cross-trip	200,000
viii) Circuit breaker 50N-Trenton, reconfigure 88S-Lingan	2,500,000
ix) System additions required for system stability and security	
x) Unforeseen impacts in NB system	
Total:	TBD

The above estimate includes the additions/changes to NSPI system only. The cost of the IC substation is not included. Items identified, to be determined (TBD), will be assessed by the SIS.

NSPI estimates the time required to construct the above facilities at 12-24 months provided that no more than 2 to 3 projects per year go forward, and assuming all easements and permits are provided and complete.

b) 138 KV Interconnection – Generating Capacity to 30 MW

Determined Cost Items	Estimate
i) Install 138 kV line terminal, 30N-Maccan	\$1,200,000
ii) Convert 37N-Parrsboro to 138 kV (7.5/10/11.2 MVA)	1,500,000
iii) Control & Communications between NSPI and customer	500,000
iv) Additions and changes to NSPI SPSs (NSPI costs only)	100,000
v) Contingency (10%)	330,000
Total of Determined Cost Item	3,630,000

To Be Determined Cost Items	<u>TBD (SIS)</u>
vi) Upgrade L-6513 to 60C (32 km)	500,000
vii) Relocate NSPI Import Power SPS cross-trip	200,000
viii) Circuit breaker 50N-Trenton, reconfigure 88S-Lingan	2,500,000
ix) System additions required for system stability and security	
x) Unforeseen impacts in NB system	
Total:	TBD

The above estimate includes the additions/changes to NSPI system only. The cost of the IC substation is not included. Items identified, to be determined (TBD), will be assessed by the SIS.

NSPI estimates the time required to construct the above facilities at 12-24 months provided that no more than 2 to 3 projects per year go forward, and assuming all easements and permits are provided and complete.

11 Preliminary Scope of SIS

The following provides a preliminary scope of work for the subsequent SIS. It will be finalized following collaboration with NBSO. This is a generic scope applicable to all generation Interconnection Requests in this northern area.

The SIS will include a more comprehensive assessment of the technical issues and requirements to interconnect generation as requested. In addition this will include contingency analysis, system stability and ride through capability and operation following a contingency (N-1 operation). The SIS must determine the facilities required to operate this facility at full capacity, withstand any first contingencies (as defined by NPCC/NERC) and identify any restrictions that must be placed on the system following a first contingency loss.

The SIS will confirm the options and ancillary equipment that the customer must install to control flicker, voltage and ensure that the facility has the required ride-through capability.

The study will identify any additional required changes to SPSs and any additional facilities required to maintain the import/export capabilities. It will include the impacts of generation that precedes this project in the NS and NB Queues. The SIS will also identify any generation that must be rejected by SPSs (new or existing) to ensure acceptable post contingency voltages, equipment loadings and system stability. The SIS will also identify any generation whose operation will be curtailed with any single element out of service.

The following outline provides the minimum scope that must be completed in order to assess the impacts. It is recognized that the actual scope may deviate, to achieve the primary objectives.

The SIS will determine the following

- Facilities that the customer must install to meet the requirements of the GIP
- The minimum transmission additions/upgrades that are necessary to permit operation of this generating facility, under all dispatch conditions, catering to the 1st contingencies listed.
- Impact on the operation of existing NS import/export and Lingan over-frequency SPS in terms of arming levels, arming means and operating limits.
- Impact on NB SPSs in southeast corridor
- Conceptual specification of any additional (proposed) SPSs
- Impact of generation addition on UFLS adequacy (forced islanding schemes)
- Impact of generation variability on SPS operation and forced islanding scheme
- Impact of generation variability on islanded operation
- Guidelines and restrictions applicable to N-1 operation (curtailments etc)
- In addition to the SPSs the UVLS systems in NB must be included in these assessments

The SIS will be based on the following bases cases

<u>Power flow base cases</u>	<u>Variations</u>
Winter Peak	import 200MW, export 200MW
Fall Peak	import 100,200,300, export 100,200,300
Summer Peak	import 100,200,300, export 100,200,300
Summer Light Load	import 100,200 export 100,250,350
	*Summer Peak export will have high NB-NE flows
	*Winter peak import case will have high NE-NB flows

In each case accommodations for the addition of wind generation will be made to the dispatch by changing the unit commitment, for that day, ensuring that sufficient capacity is available to meet the daily peak load. The assumptions regulating regulation, load following and unit commitment at the minimum daily load (two shifting etc) will be noted.

To complete this assessment the following 1st contingencies, as a minimum, will be assessed

- L-8001/L3025
- L-3006 – with and without NBPT SPS operation
- Memramcook 345/138 kV transformer
- L-6513
- L-6514
- L-6535/L-1159

- L-6536/L-1160
- L-8003
- L-8002 & L-8003 (common circuit breaker)
- L-8003 & L-8004 (common circuit breaker)
- L-8001 & 67N-T81 TX (common circuit breaker)
- L-3006 & L-3025 & Memramcook 345/138 kV Tx (common breaker)
- L-3006 & L3017 (common breaker)
- 1N-B61
- L-1108/1190 Common 138kV structure
- Loss of 180 MW of load under peak load conditions and 250 MW under light load conditions
- Loss of largest generation – Pt. Aconi 174MW net
- Loss of two generating units at Lingan – 312 Net
- Loss of the Trenton Bus (Two units with load)

To complete this assessment the dynamics of the following 1st contingencies, as a minimum, will be assessed

- 3 phase fault L-8001/3025 at 67N-Onslow, NS Import SPS operation (islanding)
- 3 phase fault L-3006 at Memramcook, NB SPS/UVLS operation (islanding)
- 3 phase fault L-3006 at Salisbury, NB SPS/UVLS operation (islanding)
- 3 phase fault L-8003 at 67N-Onslow
- 3 phase fault L-8002 at 67N-Onslow
- Slg L-3017, drops L-3017&L-3006 (common CB), NB SPS/UVLS operation,
- Slg Memramcook T3, drops L-3006 (common CB), NB SPS/UVLS operation
- Slg L-8002 at Onslow, drops L-8003, Grp5 SPS Operation
- 3 phase fault at (9N-Hopewell, drops L8003,8004, bus, SPS operation
- 3 phase fault 1N-Onslow 138 kV bus B61
- 3 phase fault 74N-Springhill 138 kV bus

After determining the changes/additions that are required to facilitate this interconnection “N-1” operation will be assessed. The objective is to determine the operating restrictions or curtailments that must be enforced to ensure secure operation of the system. This

provides a final test to ensure that the facilities are adequate and the customers business risks conveyed.

- Contingency analysis, as required
- Dynamics simulation, as required
- Determination of total generation constrained

The “N-1” assessment will include, but not be limited to, the following. The “N-1” assessment will determine the operational constraints that must be applied for “N-1” operation after the facility upgrades/additions that are recommended, for the interconnection, are constructed.